

IMPLANT FORMING BIMATERIAL MONOBLOC INTRAOCULAR LENS

The invention relates to an implant forming an intraocular lens and intended for implantation in the eye of a patient who is lensed or lensless (aphacic) following extraction of the opacified natural crystalline lens, or for correction of refractive ametropias.

In the case of an eye which is aphacic following opacification of the natural crystalline lens (cataract) the implant is generally placed in the posterior chamber in the capsular sac situated behind the iris, but can also be implanted in the ciliary sulcus or in the anterior chamber in front of the iris.

In the case of a lensed eye, implantation with the aim of correcting a refractive ametropia generally takes place in front of the iris, since the capsular sac is still occupied by the natural crystalline lens. However, it is also possible to envisage implantation behind the iris, between the iris and the crystalloid substance.

All implants which form an intraocular lens include a central optical part, whose overall contour is circular, and a haptic part, which is disposed at the periphery of the optical part and is intended to be positioned so as to stabilize the implant.

Numerous types of implants referred to as rigid implants are known, commonly being made of polymethyl methacrylate (PMMA). Such implants require a major sclerocorneal incision and risk damaging the ocular tissues.

In order to overcome this problem, attempts have been made to develop implants referred to as flexible implants, made in particular of hydrogel, hydroxyethyl methacrylate (HEMA) and flexible acrylic material. These implants can be folded or rolled up on themselves, in particular about a diametral axis of the optical part, for

introduction via a small incision, allowing rapid sclerocorneal cicatrization.

One known flexible implant comprises a central, lens-forming optical element and two haptic elements at the periphery of the optical element. With flexible implants of this type, made in particular of hydrogel, hydroxyethyl methacrylate (HEMA) and flexible acrylic material, the problems of positioning and stabilization are more difficult to solve than with other, rigid implants.

In the case of implantation following extraction of the opacified crystalline lens, it is known that the implants are difficult to maintain in a stable position owing to the fact that the cut made in the anterior capsule is not, in practice, perfectly centered. The cut edge of said anterior capsule therefore covers the haptic branches to differing extents. Consequently, in the weeks following the operation, the axial component of the force which is exerted by contraction of the cut edge of the anterior capsule on a haptic element can vary depending on the position of the implant in the capsular sac. One of the haptic branches can be drawn backward, such that correct positioning of the implant in the capsular sac is not ensured.

Likewise, in the case of implantation in a lensed eye, the position of the implant must be stable in order to prevent any displacement or contact of certain parts of the implant with the internal eye tissues.

In an attempt to resolve these difficulties, the production has been considered of bimaterial intraocular implants, i.e., implants comprising an optical part in a first material, generally flexible, allowing folding and rolling, and haptic parts made of a second, rigid material, such as PMMA, in order to ensure a good hold and stability of the lens following implantation.

EP208546 describes an implant comprising an optical

part made of PMMA and a haptic part, made of polypropylene, at the periphery of the optical part. Subsequently, mechanical integration is ensured by virtue of a laser beam which softens the material, which subsequently hardens after cooling. An operation of this kind is complicated and considerably increases the production costs of the lens.

Also known is an intraocular lens comprising an optical part made of flexible material and a haptic part made of rigid material, such as PMMA, which ensures bonding by fusion of the two materials in the contact zone. The process of manufacture of such a lens likewise exhibits disadvantages. Specifically, the positioning of the haptic parts relative to the periphery of the optical part is not easy, so leading to an increase in the manufacturing costs of the lens. Defects may also become evident at the junction zone, bringing with them a risk of separation of the haptic part.

One object of the invention is to provide an implant which forms an intraocular lens and which suffers neither from the disadvantages of monobloc intraocular lenses made from rigid material or flexible material nor from the disadvantages of bimaterial implants which involve the fusion or assembly of the haptic and optical parts.

The implant for a lensed or aphacic eye, according to the invention, comprises:

an optical part and a haptic part, the optical part being made at least partially of flexible material and the haptic part being made at least partially of rigid material, wherein the structure of said implant is monobloc.

According to one provision of the invention, the rigid material is the flexible material in a form modified by at least one reaction selected from chemical reactions and polymerization reactions.

The optical part can be made entirely of flexible

material or can comprise one or more strips made of flexible material alternating with strips made of rigid material. Whatever the embodiment, the rigid material of the optical part allows said part to be folded or rolled in order that it can be introduced through a small incision.

In accordance with one variant embodiment, the optical part comprises a zone made of rigid material which adjoins the haptic part and is in continuity with the rigid material of the optical part.

In practice, the haptic part will be made entirely of rigid material. It may comprise one (or more) zone(s) made of flexible material.

The flexible material of the implant which forms an intraocular lens is generally hydrophilic, but may also be selected from polysiloxanes, which are not (generally) hydrophilic; their flexibility is due to a very low glass transition temperature (T_g).

The flexible material of the implant which forms an intraocular lens is advantageously selected from crosslinked polymer and copolymer materials such as, for example, random methyl methacrylate-hydroxymethyl methacrylate (MMA-HMA) copolymers crosslinked by the addition of a polyfunctional agent such as diethylene glycol dimethacrylate. The flexible material of the lens is based, for example, on PMMA-PHMA copolymers, crosslinked with diethylene glycol dimethacrylate.

The implant of the present invention is notable in that it is both monobloc and bimaternal. The rigid material results from a structural modification of the flexible material. The implant of the invention thus consists of two materials, a flexible material and a rigid material, without any fusion or assembly of these two materials.

The combination of the two features, monobloc and bimaternal, in the implant according to the invention gives it a reliability and a longevity which are superior to

those of known bimaterial lenses made by fusion or assembly.

The process of manufacturing the implant comprises a first step of producing a preform (or blank) which can be shaped into an intraocular lens from a flexible monobloc starting material, a step of shaping of said preform into an intraocular lens, characterized in that said process further comprises a step of structurally modifying at least one zone of the preform which it is intended should become rigid.

In accordance with one provision of the invention, the step of structural modification comprises a phase of impregnating the zone of the preform with reactive organic compounds.

The step of structurally modifying the starting material can be carried out by deploying a chemical reaction and/or a polymerization reaction.

In a first embodiment of the invention, the shaping step, which is commonly carried out by machining, precedes the step of structurally modifying the starting material. In such a case, it is appropriate to carry out a step of protecting at least one zone of the preform which it is intended should remain flexible, prior to the step of structurally modifying the starting material, and then to remove protection from this zone of the preform which it is intended should remain flexible.

In accordance with another embodiment of the invention, the shaping step (machining) follows the structural modification step.

The process of the invention therefore breaks down into four distinct steps:

- premachining step (production of a preform or blank)
- selective impregnation step
- step of modification by chemical reaction and/or

polymerization

- step of removing protection or machining (shaping of the preform).

5 A number of approaches can be used, individually or in combination:

- chemical reaction between a monofunctional or polyfunctional compound and a reactive element of the material of the lens.

10 - polymerization of one or more monomers within the material of the lens.

- polymerization of a mixture of monomers and polymers outside the material of the lens.

15 In accordance with a first embodiment of the invention, the anchoring of groups on the material of the lens and/or the formation of an interpenetrated polymer network makes it possible to modify, durably and irreversibly, the characteristics of the modified zone which it is intended should constitute the rigid part, and, in particular, to increase its rigidity (increase in modulus, reduction in hydrophilicity, etc.).

20 In accordance with another embodiment of the invention, the anchoring of functional groups on the material of the lens allows copolymerization with a mixture of monomers and/or polymers (formation of MOPO).

25 In the case of MMA-HMA copolymers, for example, it is possible to utilize the reactivity of the hydroxyls of HMA units in order to attach groups capable of modifying the characteristics of the material.

30 In this case, the possible reactions can be grouped into five categories:

- the reactive compound used is monofunctional. Its reaction with the reactive functions of the material of the lens results in chemical modification of the structure of the material and in a decrease in its hydrophilicity. By way of example, mention may be made of functional monomers

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heterocyclic monomers such as propylene oxide, etc.

- the reactive compound used is polyfunctional. One or more of its functions are antagonistic to the functions of the material and are capable of reacting with them. The remaining function or functions is or are copolymerizable with a mixture of monomers and/or a polymer blend. By way of example, the reactive compound can be methacrylic acid, acrylic acid or an alkylacryloyl halide (methacryloyl chloride in particular), it being possible for the mixture of monomers to be a mixture of styrene, acrylic and alkylacrylic derivatives and it being possible for the polymers to be PMMA, poly(methyl methacrylate-co-styrene), poly(methyl methacrylate-co-alkyl acrylate) and poly(methyl methacrylate-co-alkylacrylate) and poly(methyl methacrylate-co-alkyl alkylacrylate). The monomer mixture/polymer blend is combined with a free-radical initiator.

So as to penetrate the interior of the material, in order to modify it right through, the reactive compounds must, preferably, be miscible with the copolymer chains and must, consequently, possess an appropriate chemical structure.

On premachined lenses it is also possible to carry out surface modification of the zone or zones to be rigidified. Under these conditions, however, the properties obtained are less satisfactory.

The partial and selective impregnation of a specific zone of the lens (which it is intended should become the rigid part) requires the part which it is intended should remain flexible not to be in contact with the reactive compounds. This can be realized in a number of ways:

- in the case of ready-machined lenses, by protecting the part of the lens which it is intended should remain flexible by a temporary impermeable coating, which

is subsequently removed;

- in the case of preformed blanks, by an appropriate cutout, which ought to allow rapid impregnation by diffusion of the organic reactive compounds into the zone to be rigidified, which it is intended should become the rigid part, in particular by cutting or premachining thereof. The part which ought to remain flexible, which is not machined, is protected by an overthickness of material, said material preventing the diffusion of the organic reactive compounds to the core of the material which will constitute the flexible part of the lens.

The part which has remained flexible is, finally, exposed by machining following the steps of impregnation and chemical reaction.

In accordance with a first embodiment of the invention, the impregnating step is carried out with an impregnating solution composed, for example, of methacryloyl halide, (in particular, methacryloyl chloride) and a free-radical initiator such as benzoyl peroxide, or of a mixture of methyl methacrylate, acrylic acid, methacryloyl chloride, ethylene glycol dimethacrylate and a free-radical initiator such as azo(bis)isobutyronitrile.

The impregnating step is commonly carried out at ambient temperature, at approximately 20°C, for a period of from 1 h to 48 h, depending on the thickness of the zone to be rigidified, and on the desired rigidity. Increasing the temperature makes it possible to reduce the impregnation time.

In accordance with another embodiment of the invention, the impregnating solution is composed exclusively of a polyfunctional compound such as methacrylic acid or an alkyacryloyl halide (especially methacryloyl chloride).

The modification step is carried out by adding a mixture of monomers and/or a polymer blend in combination

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with a free-radical initiator. The copolymerization temperature is between 20 and 95°C for a period of from 1 h to 48 h.

5 The step of structural modification by chemical reaction and/or polymerization reaction is carried out under an inert atmosphere at a temperature of between 30°C and 95°C. A pressure of approximately 1 to $5 \cdot 10^5$ Pa makes it possible to limit the evaporation of the reactants.

10 The duration of this step is between a few minutes and 48 h, depending on the temperature and on the nature of the catalyst or initiator which is used. The hardness or rigidity which is required for the rigid part is a function of the rate of the chemical modification and/or polymerization reaction.

15 Regarding the chemical reactions which lead to structural modification of the material, Lewis acids and bases can be used as catalysts. By way of example, mention may be made of the catalysts BF_3 , TiCl_4 , amines, etc.

20 Free-radical polymerization initiators are usually employed for polymerization reactions. By way of example, mention may be made of peroxides, hydroperoxides, percarbonates, redox couples, azonitriles, etc. The initiators used must possess, preferably, a chemical structure which is adapted so as to diffuse into the chains
25 of the material and must have a half-life which is compatible with the chosen polymerization temperature and polymerization time.

30 The step of removing protection from the protected part of the lens, in the case of premachined lenses, or the machining of the blank, makes it possible to create a nonmodified flexible part and a rigidified zone.

35 The process of the invention for structural modification by selective rigidification, described above, makes it possible to obtain implants featuring haptic parts having attachment members of various geometric shapes,

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attachment members having damping elements, or flat haptic parts or other haptic parts of any desired configuration.

The lenses are subsequently placed in an aqueous medium in order to induce the swelling of the flexible part and to remove the unreacted products by washing.

The process of the invention will also be described by means of the following nonlimiting examples.

The starting lenses are flexible lenses based on PMMA-PHMA copolymers whose characteristics are as follows:

- HMA content: approximately 60 molar %
- MMA content: approximately 40 molar %
- ethylene glycol dimethacrylate: approximately 0.25 molar %
- in aqueous medium, the degree of swelling is 28%.

Example 1

The impregnating solution is composed of 3 ml of methacryloyl chloride. Impregnation is carried out by soaking the preform at 20°C for from 4 to 24 h depending on the thickness of the part to be rigidified and the rigidity desired.

Example 2

The impregnating solution is composed of 3 ml of methacryloyl chloride and 300 mg of benzoyl peroxide. Impregnation is carried out by soaking the preform at 20°C for from 4 to 24 h depending on the thickness of the part to be rigidified and the rigidity desired.

Example 3

The impregnating solution is composed of 1.5 ml of methyl methacrylate, 1.5 ml of methacryloyl chloride and 300 mg of benzoyl peroxide. Impregnation is carried out by soaking the preform at 20°C for from 4 to 24 h depending on the thickness of the part to be rigidified and the rigidity desired.

Example 4

The impregnating solution is composed of 2.7 ml of

methacryloyl chloride, 0.3 ml of ethylene glycol dimethacrylate and 300 mg of benzoyl peroxide. Impregnation is carried out by soaking the preform at 20°C for from 4 to 24 h depending on the thickness of the part to be rigidified and the rigidity desired.

Example 5

The impregnating solution is composed of 2.4 ml of acrylic acid, 0.6 ml of methacryloyl chloride and 300 mg of benzoyl peroxide. Impregnation is carried out by soaking the preform at 20°C for from 4 to 24 h depending on the thickness of the part to be rigidified and the rigidity desired.

Example 6

The impregnating solution is composed of 2 ml of methyl methacrylate, 0.7 ml of acrylic acid, 0.3 ml of ethylene glycol dimethacrylate and 300 mg of azo(bis)isobutyronitrile. Impregnation is carried out by soaking the preform at 20°C for from 4 to 24 h depending on the thickness of the part to be rigidified and the rigidity desired.

The step of structural modification by chemical reaction and/or polymerization is carried out under an inert atmosphere at a pressure of approximately $2 \cdot 10^5$ Pa. The duration of this step is between 4 and 24 hours depending on the desired rigidity or hardness and in accordance with the amount of polymerization- or reaction-initiating agent which is present in the medium, and in accordance with the desired rigidity for the rigid part.

The step of protecting the flexible part of the lens, in the case of premachined lenses, or the machining of the blank, makes it possible to create a nonmodified part, which has remained flexible, and a zone which has become rigid.

In one embodiment, only the haptic parts or the portions in which the haptic parts are to be formed are

impregnated. In a variant embodiment, zones of the optical part adjoining the haptic parts may also be impregnated. Similarly, one or more strips, parallel to a diameter, for example, can be impregnated, strips alternating with the aforementioned strips being protected so as to remain flexible. It will be understood that such strips allow the optical part to be folded or rolled around the zones which have remained flexible.

Example 7

The impregnating solution is composed of 1.5 ml of methacryloyl chloride. The duration of impregnation is 4.5 h. The step of copolymerization is carried out by adding a mixture of PMMA and methyl methacrylate, n-butyl methacrylate and benzoyl peroxide.

Example 8

The impregnating solution is composed of 1.5 ml of methacryloyl chloride. The duration of impregnation is 4.5 h. The step of copolymerization is carried out by adding a mixture of PMMA and methyl methacrylate, n-butyl methacrylate, hydroxyethyl methacrylate and benzoyl peroxide.

Example 9

The impregnating solution is composed of 1.5 ml of methacryloyl chloride. The duration of impregnation is 4.5 h. The step of copolymerization is carried out by adding a mixture of PMMA and methyl methacrylate, n-butyl methacrylate, hydroxyethyl methacrylate, ethylene glycol dimethylacrylate and benzoyl peroxide.

Example 10

The impregnating solution is composed of 1.5 ml of methacryloyl chloride. The duration of impregnation is 4.5 h. The step of copolymerization is carried out by adding a mixture of poly(methyl methacrylate-co-styrene), methyl methacrylate, n-butyl methacrylate, ethylene glycol dimethylacrylate and benzoyl peroxide.

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